

# Calibration of Air-Coupled Transducers for Absolute Nonlinear Ultrasonic Measurements

Nicholas Selby<sup>1</sup>, Undergraduate Research Assistant

David Torello<sup>1</sup>, Jin-Yeon Kim<sup>2</sup>, Laurence J. Jacobs<sup>1,2</sup>

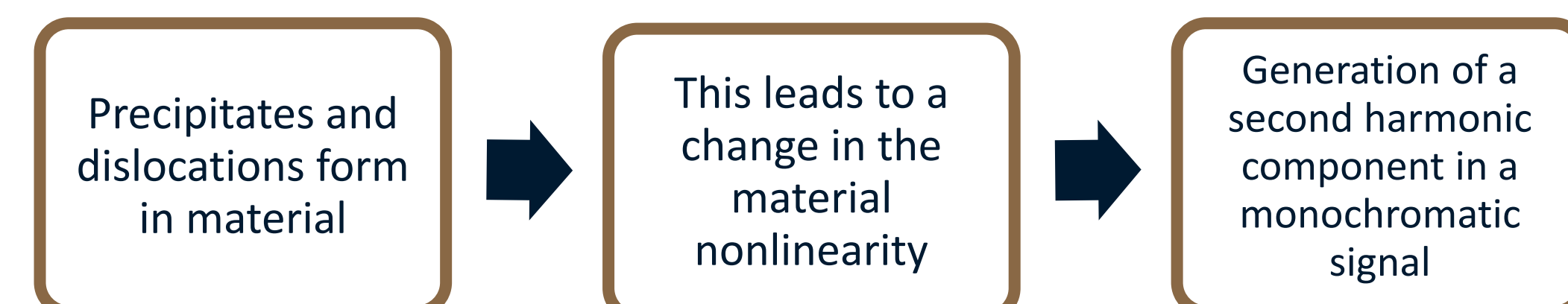
<sup>1</sup>G.W. Woodruff School of Mechanical Engineering, Georgia Institute of Technology, Atlanta, GA, 30332

<sup>2</sup>School of Civil and Environmental Engineering, Georgia Institute of Technology, Atlanta, GA, 30332

## Motivation

### Absolute Nonlinear Ultrasonics (NLU)

- Absolute NLU has the potential to **detect material degradation** and provide quantitative information about substructural changes in a material



- Current noncontact measurement techniques are **relative**. They can only be used if the complete history of the specimen **is already known**
- Absolute** measurement techniques can determine nonlinear material parameters for materials with no measurement history

### Air-Coupled Transduction

- Air-coupled transducers are preferable for their **low cost and greater robustness** over other receiver technologies due to lack of dependence on contact and surface conditions
- Air-coupled transducers must be **calibrated** in order to provide absolute measurement data
- Standard pulse-echo (self-reciprocity) calibration doesn't work because of low power output from the transducer

## Objectives

- Calibrate** an air-coupled transducer by experimentally identifying its force/voltage transfer function with a model-based, pitch-catch experimental configuration
- Confirm** calibration with laser interferometer measurements of excited material surface

## Theoretical Background and Methods

### Second Harmonic Generation

- Material nonlinearity** is measured when material defects and microstructural effects cause a monochromatic wave to **distort** into a **fundamental ( $\omega$ )** and **second harmonic ( $2\omega$ )** component
- For longitudinal waves, material nonlinearity is denoted by  $\beta$  and adheres to the relationship:

$$\beta = \frac{8A_2}{A_1^2 k^2 x}$$

$A_1$  and  $A_2$  denote absolute amplitudes of fundamental and first harmonic wave frequency components

### Multiple Gaussian Beam Modelling

- Computationally efficient method to model longitudinal wave propagation
- Source velocity expressed as sum of Gaussians, which **propagate as Gaussians**:

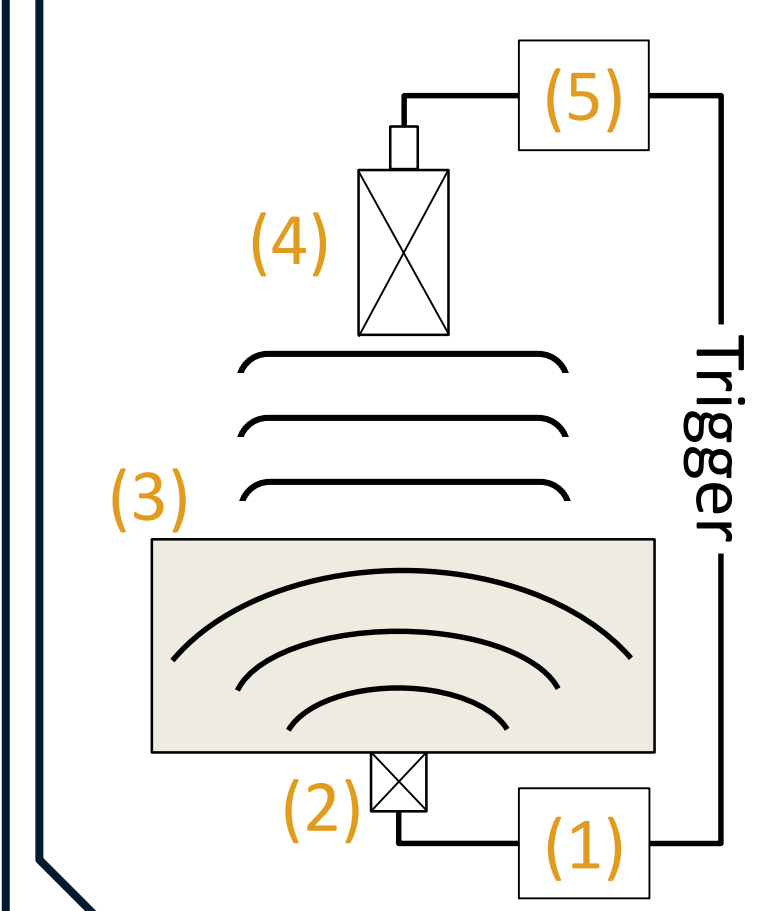
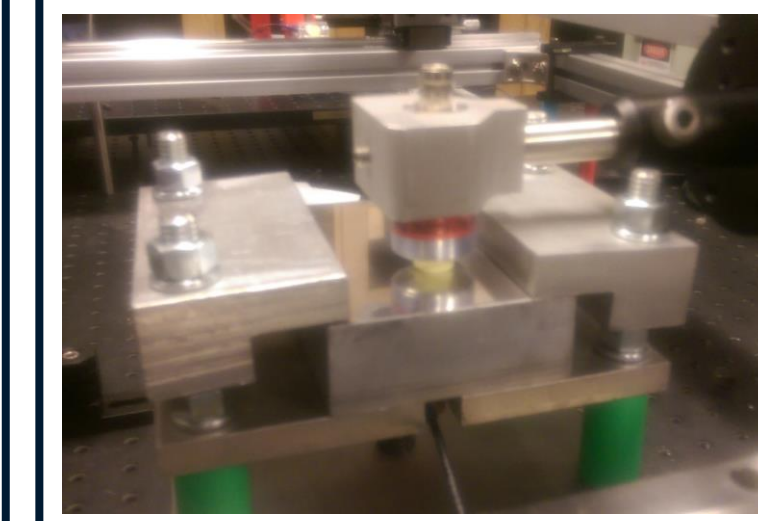
$$V_0(\xi) = \sum_{n=1}^{N=15} A_n \exp\left(-\frac{B_n r^2}{a^2}\right)$$

- Source velocity is translated to pressure** via the following relationships:

$$\begin{aligned} \tilde{p}_1(z) &= [p_0 \exp(ikz)] [M_1(\alpha_1, z)] [D_1(a, f, z)] & \tilde{p}_2(z) &= \left[ \frac{\beta k z}{2\rho_0 c_0^2} p_0^2 \exp(2ikz) \right] [M_2(\alpha_1, \alpha_2, z)] [D_2(a, 2f, z)] \\ M_1(\alpha_1, z) &= e^{-\alpha_1 z} & M_2(\alpha_1, \alpha_2, z) &= \frac{e^{-2\alpha_1 z} - e^{-\alpha_2 z}}{(\alpha_2 - 2\alpha_1)z} \\ D_1(a, f, z) &= \sum_{m=1}^N \frac{A_m}{1 + iB_m z / D_R} \exp\left(\frac{i\omega}{2} \frac{iB_m / c_0 D_R}{1 + iB_m z / D_R} r^2\right) & D_2(a, 2f, z) &= \frac{1}{z} \int_0^z \sum_{n=1}^N \sum_{m=1}^N \frac{2A_n A_m}{(2 + B_a z) + (B_a - 2B_b z)z'} \exp\left(\frac{ikr^2(B_a - 2B_b z')}{(2 + B_a z) + (B_a - 2B_b z)z'}\right) dz' \end{aligned}$$

- Pressure is then integrated over transducer surface to calculate **received force for calibration**

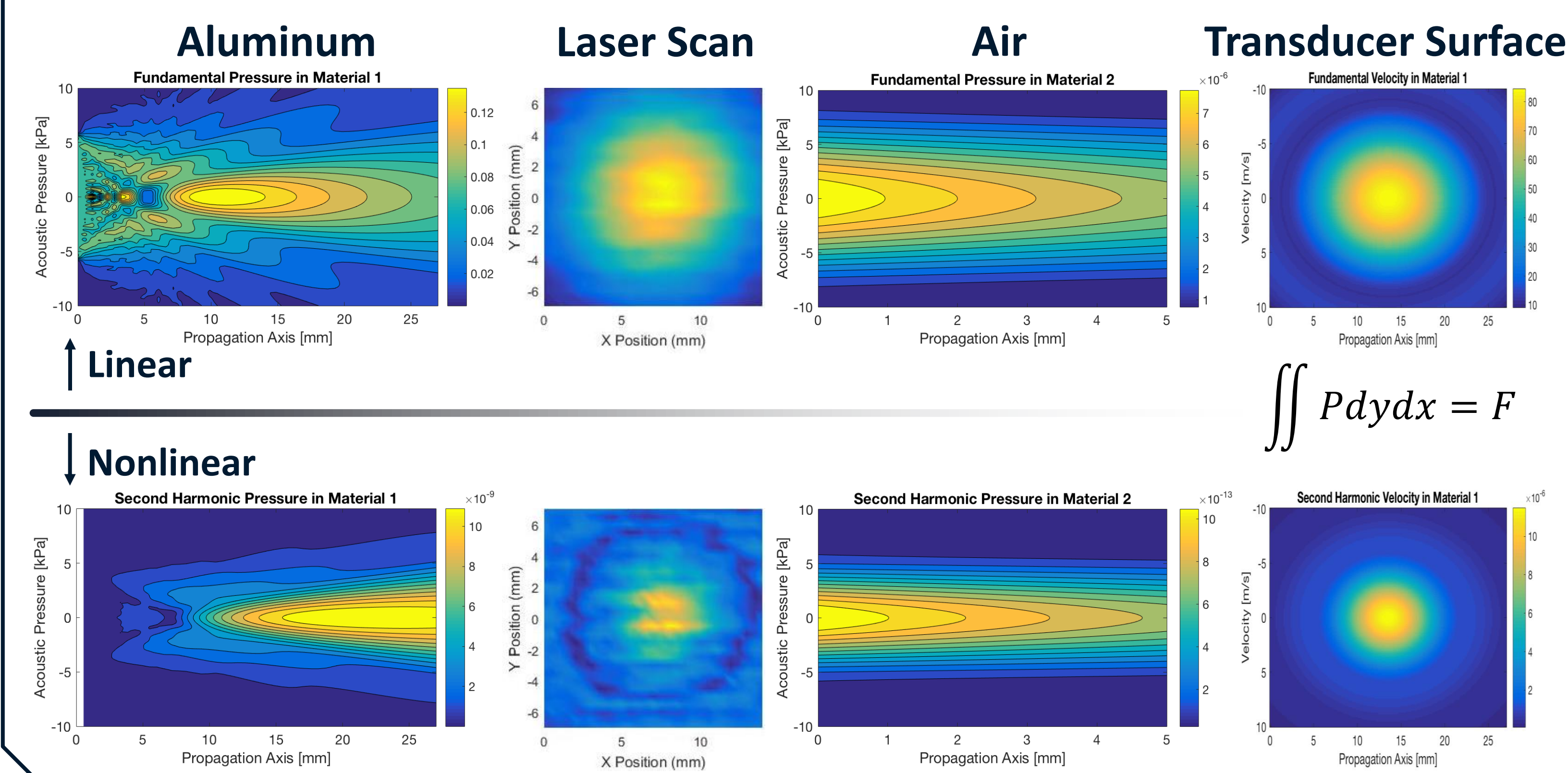
### Experimental Setup



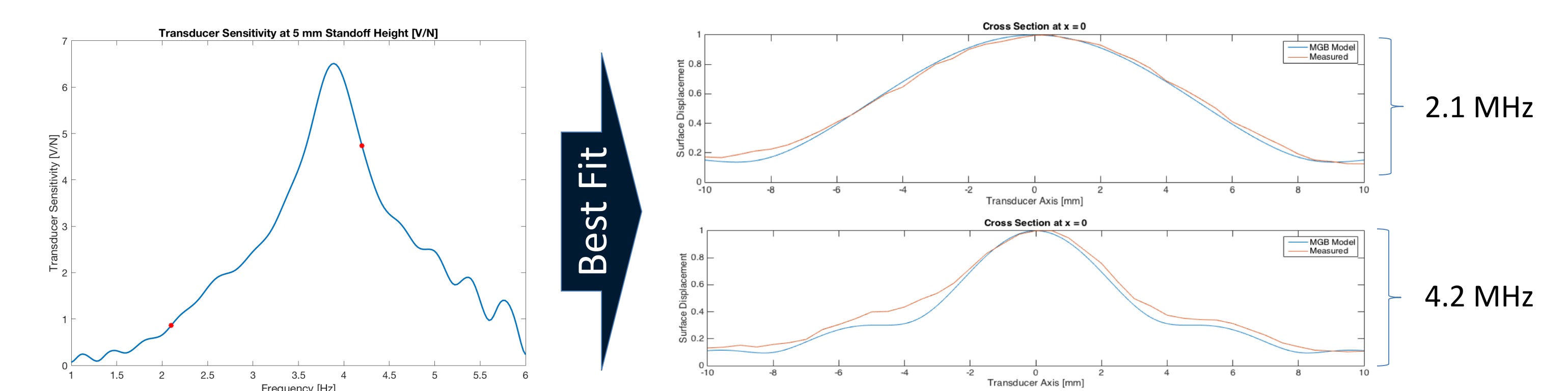
- RITEC 2500GA: Sinusoidal **signal generation** (1.8 MHz, 12 cycles)
- Lithium niobate **transducer**: Excitation of longitudinal wave in material, oil-coupled
- Material **Sample**: Aluminum 2024 or Fused Silica
- Ultran NCT4-D6 **air-coupled transducer**: Detection of plane wave
- Oscilloscope: Tektronix TDS5034B **Digital Oscilloscope**

## Results and Discussion

### Measurement Results



### Data Fitting and Extraction of $\beta$



- Window time-domain waveform to **extract steady state signal**
- Waveform undergoes FFT to **extract amplitudes  $A_1$  and  $A_2$** , fundamental and first harmonic frequencies
- Plot transducer transfer function
- Employ best fit optimization to **calibrate transducer parameters**

$$\beta = 5.1$$

Values in literature range from 5 to 9.

**Agrees with literature!**

### Conclusions

- Air-coupled transducers **can be calibrated inexpensively** using a contact transducer and a material with known nonlinear properties
- A **computational multiple Gaussian beam model** is provided and confirmed by laser interferometer results from material surface vibrations
- Measurement of  $\beta$  **matches expected value from literature**

### References

- K. H. Matlack, J.-Y. Kim, J. Wall, J. Qu, and L. Jacobs. Proceedings of Meetings on Acoustics, 19, 045023, 2013.
- D. J. Shull, E. E. Kim, M. F. Hamilton, and E. A. Zabolotskaya. JASA, 97(4):2126–2137, 1995.
- J. Wen, M. Breazeale. JASA, 83(5):1752–1756, 1988.